

Pavement Design Guide to Pavement Technology Parts 2 and 4C 9 March 2018



Today's moderator

Eliz Esteban

Communications Officer Austroads

P: +61 2 8265 3302

E: <u>eesteban@austroads.com.au</u>





About Austroads



The peak organisation of Australasian road transport and traffic agencies

- Roads and Maritime Services New South Wales
- Roads Corporation Victoria
- Department of Transport and Main Roads Queensland
- Main Roads Western Australia
- Department of Planning, Transport and Infrastructure South Australia
- Department of State Growth Tasmania
- Department of Transport Northern Territory
- Transport Canberra and City Services Directorate, Australian Capital Territory
- Commonwealth Department of Infrastructure, Regional Development and Cities
- Australian Local Government Association
- New Zealand Transport Agency

Our structure



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| Project Delivery Task Force | | , and | | | | |

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Pre Qu

Presentation = 40 minsQuestion time = 10 mins



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Today's presenter

Dr Michael Moffatt

National Technical Leader Pavements and Surfacings ARRB

P: +61 3 9881 1650

E: michael.moffatt@arrb.com.au





Agenda

| Торіс | Presenter |
|--|-----------------------|
| Project Background and Introduction | |
| Guide to Pavement Technology Part 2: Pavement Structural Design Lime Stabilised Subgrades Cemented Materials Lean-mix Concrete Asphalt Characterisation Design Traffic Axle Strain Method (ME bound materials) | Dr Michael Moffatt |
| Guide to Pavement Technology Part 4C: Materials for Concrete Road Pavements | |
| Q&A | |





Project Background and Introduction





Evolution of Guide to Pavement Technology Part 2



12

2017 Edition

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2017

Part 2: Pavement Structural Design









2002 – 2018 Reports



Introduction to Team



Project Team



Austroads Project Manager Andrew Papacostas VicRoads



Project Leader Michael Moffatt ARRB



Team Member Geoff Jameson ARRB

Review Team





Austroads Pavements Task Force



Stakeholders -Road & Traffic Authorities & Industry



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Guide to Pavement Technology Part 2 Pavement Structural Design



Overview of Part 2 changes





Flexible pavements

- Lime stabilised subgrades
- Cemented materials
- Lean-mix concrete
- Asphalt
- Design traffic
- Removal of Standard Axle Repetitions (SARs)
- Axle-strain method

Rigid pavements

• Joint detailing diagrams



Lime Stabilised Subgrades



Lime Stabilised Subgrades





2012

 Lime stabilised subgrades not

structural



AP-R435-13

2013

- Researched methods
- Lime stabilised subgrades
 - = selected subgrades
 - ≠ subbase layers
- ME procedure
- Empirical procedure

Adoption in 2017

Only applicable if:

- Lime provides long term strength
- Lime content meets lime demand test (lime content when pH = 12.4)
- Minimum CBR of 60%

Allows maximum E = 150 MPa

Lime stabilised subgrade considered in same way as selected materials







Cemented Materials







- In situ flexural modulus
 - after 28 days curing in roadbed
- Estimated
 - Unconfined Compressive Strength (UCS) tests
 - Presumptive values





- In situ flexural modulus
 - after 90 days curing in roadbed
- Measured
 - -4-point flexural beam
 - Lab-field adjustment factor
- Estimated
 - Unconfined Compressive Strength (UCS) tests
 - Presumptive values





- Applied tensile strain
- Modulus
- Project reliability

$$N = RF \left[\frac{\frac{113000}{E^{0.804}} + 191}{\varepsilon} \right]^{12}$$





4-point Beam Testing: Modulus







4-point Beam Testing: Modulus + Strength







3 methods
$$\sqrt{}$$
 Same as 2012
 $N = RF\left(\frac{K}{\varepsilon}\right)^{12}$

- 1. Fatigue measurements (inc. lab-field factor)
- 2. Estimated from measurements of flexural strength & modulus (inc. lab-field factor)
- 3. Presumptive values (No RF)



Lean-mix Concrete



Cemented materials





Cemented materials type included lean-mix concrete

$$N = RF \left[\frac{\frac{113000}{E^{0.804}} + 191}{\varepsilon} \right]^{12}$$

2017 Cemented materials





- Lean-mix concrete a separate material type
- Presumptive values



Asphalt Characterisation







Estimate of the value obtained from either:

- Resilient modulus measured using the standard indirect tensile test (ITT) adjusted to in-service temperature and rate of loading
- Estimation from bitumen properties using Shell nomographs and in-service temperature and rate of loading



Guide to Pavement Technology Part 2 Pavement Structural Design Austroad

- Retains both methods
- Clarifies that both yield a flexural modulus (built into rate of loading adjustment)
- Adds direct measurement of flexural modulus





- Flexural modulus measurement at inservice speed and temperature (WMAPT)
- Interpolation from measured flexural modulus over a wide range of speed and temperatures
- 3. Measure ITT as in 2012 Guide
- Estimation from Shell nomographs as in 2012 Guide









$$N = \frac{SF}{RF} \left[\frac{6918(0.856V_b + 1.08)}{E^{0.36}\varepsilon} \right]^5$$

Presumptive SF = 6

| Desired project reliability | | | | | |
|-----------------------------|-----|-----|-----|-----|-------|
| 50% | 80% | 85% | 90% | 95% | 97.5% |
| 1.0 | 2.4 | 3.0 | 3.9 | 6.0 | 9.0 |





- Guidance on using laboratory measured fatigue performance in design
- Requires understanding relationship between lab and field performance

| WMAPT (°C) | ≤ 25 | 26 - 34 | ≥ 35 |
|----------------------------|---------------------|---------------------|-----------------|
| Design traffic limit (ESA) | 4 x 10 ⁸ | 2 x 10 ⁸ | 10 ⁸ |

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Design Traffic





2017 Capacity Check



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Check that:

Annual number of Heavy Vehicles ≤ lane capacity

Simple approach adopted:

Capacity is when flows mean that road is saturated 24 h/day



Axle Strain Method Mechanistic Empirical (ME) Bound Materials



2012 Axle Strain Method (ME Bound Materials)



- Calculate strain only under a 80 kN Standard Axle load
- Calculate allowable traffic loading under 80 kN Standard Axle load
- Design traffic needed to be expressed in terms of repetitions of a Standard Axle
- Cumulative traffic over design period includes various axle group types and loads



2012 Axle Strain Method (ME Bound Materials)

- From strains calculate the <u>allowable loading</u> in terms Standard Axle Repetitions
- Hence, express the <u>design traffic</u> in Standard Axles Repetitions of damage



| Axle | Proportion of load levels by axle group type [%] | | | | | |
|------------|--|------------|--------------|------------|------------|------------|
| group load | Single | Single | Tandem | Tandem | Triaxle | Quad-axle |
| [kN] | single-tyres | dual-tyres | single-tyres | dual-tyres | dual-tyres | dual-tyres |
| 10 | 0.0101 | 1.0001 | | 0.0900 | | |
| 20 | 1.2666 | 1.5502 | | 0.2100 | 0.0200 | |
| 30 | 12.5342 | 13.5614 | | 0.4600 | 0.0300 | |
| 40 | 13.9123 | 14.6415 | 0.0414 | 1.7100 | 0.1100 | |
| 50 | 13.8717 | 14.8615 | 0.1448 | 2.5000 | 0.6000 | |
| 60 | 18.4011 | 13.5814 | 1.5517 | 4.1100 | 2.0900 | 0.5539 |
| 70 | 20.6708 | 10.5511 | 5.6481 | 5.7500 | 3.6800 | 0.5539 |
| 80 | 14.8445 | 9.1009 | 9.0824 | 7.0100 | 5.2800 | 0.3728 |
| 90 | 4.4888 | 7.1007 | 8.7825 | 6.8800 | 5.6500 | 2.2262 |
| 100 | | 5.3405 | 10.6031 | 6.2500 | 5.2800 | 5.9438 |
| 110 | | 3.7704 | 13.1271 | 5.6300 | 4.8400 | 9.8530 |
| 120 | | 2.3202 | 13.5306 | 4.7000 | 4.3200 | 18.4065 |
| 130 | | 1.4901 | 14.1202 | 4.7600 | 4.3300 | 12.6438 |
| 140 | | 0.7801 | 10.9341 | 4.7000 | 3.8800 | 5.3899 |
| 150 | | 0.3500 | 6.6205 | 4.9700 | 3.8900 | 2.7908 |
| 160 | | | 3.7550 | 5.5600 | 4.1600 | 2.5991 |
| 170 | | | 2.0585 | 5.4800 | 3.9000 | 2.0452 |
| 180 | | | | 5.7200 | 4.3000 | 0.7456 |
| 190 | | | | 5.1800 | 4.3000 | 1.6723 |
| 200 | | | | 4.8500 | 4.6000 | 1.2995 |
| 210 | | | | 4.4200 | 5.2400 | 0.5539 |
| 220 | | | | 3.2700 | 5.1800 | 1.1184 |
| | | | | A 4544 | F 7000 | 1 2005 |

equivalent Standard Axle Repetitions

2012 Axle Strain Method (ME Bound Materials)





| Axle type | Standard group load [kN] |
|----------------------------|-----------------------------|
| single axle – single tyres | 53 |
| single axle – dual tyres | 80 |
| tandem – dual tyres | 135 |
| triaxle – dual tyres | 181 |
| quad-axle – dual tyres | 221 |

| Distress type | LDE |
|--------------------------------|-----|
| asphalt fatigue | 5 |
| cemented material /LMC fatigue | 12 |
| rutting and shape loss | 7 |

Shortcomings of 2012 Method



- Standard loads used to determine SAR independent based on equal deflection
- Standard loads assumed equal maximum deflection equals equal damage
 - Regardless of number of occurrences of that deflection (i.e. Axles with group)
- Design method equates damage to strains not deflections
- Standard loads independent of structure
 - Strains vary with pavement structure



2017 Method

- Design traffic expressed as the expected number of repetition for each axle load on each axle group type
- Allowable loading in terms of fatigue damage - calculated for each axle load on each axle group type
- Fatigue damage calculated by dividing the expected repetitions by the allowable repetitions

| Axle group load (kN) | Expected group repetitions | Axles in group | Critical strain (microstrain) | Allowable group repetitions | Damage |
|-------------------------|-------------------------------|----------------|----------------------------------|--------------------------------|----------|
| 10 | 66 334 | 1 | 21.9 | 2.06E+11 | 1.14E-09 |
| 20 | 166 0 94 | 1 | 43.8 | 6.42E+09 | 1.45E-07 |
| 30 | 448 086 | 1 | 65.6 | 8.46E+08 | 1.19E-06 |
| 40 | 418 863 | 1 | 87.5 | 2.01E+08 | 1.59E-05 |
| 50 | 320 880 | 1 | 109.4 | 6.58E+07 | 1.60E-04 |
| 60 | 183 475 | 1 | 131.3 | 2.64E+07 | 5.82E-04 |
| 70 | 124 150 | 1 | 153.1 | 1.22E+07 | 1.45E-03 |
| 80 | 88 299 | 1 | 175.0 | 6.27E+06 | 2.52E-03 |
| 90 | 56 708 | 1 | 196.9 | 3.48E+06 | 3.54E-03 |
| 100 | 26 606 | 1 | 218.8 | 2.06E+06 | 5.70E-03 |
| 110 | 7 827 | 1 | 240.6 | 1.28E+06 | 7.95E-03 |
| 120 | 2 212 | 1 | 262.5 | 8.26E+05 | 1.17E-02 |
| 130 | 466 | 1 | 284.4 | 5.54E+05 | 1.72E-02 |
| | | | | Total SADT damage | 0.271 |

Table L 11: Calculation of asphalt damage - single axle/dual tyres (SADT) - full depth asphalt pavement



2017 Method



• Consistent with method used for concrete pavements

| SINGLE AXLES / SINGLE WHEELS (SAST) | | | | | | |
|-------------------------------------|---------------------|-------------------------|--------------------------|-------------|--------------------------|------------|
| | | | Equivalent Stress | 0.726 | | |
| | | | Stress Ratio Factor | 0.171 | Erosion Factor | 1.837 |
| | | | Fatigue Ana | lysis | Erosion An | alysis |
| Axle Load (kN) | Design Load (kN) | Expected Repetitions | Allowable Repetitions | Fatigue (%) | Allowable Repetitions | Damage (%) |
| 130 | 169.0 | 2,361 | 5,668 | 41.66 | 197,614 | 1.19 |
| 120 | 156.0 | 4,990 | 21,487 | 23.23 | 331,752 | 1.50 |
| 110 | 143.0 | 7,673 | 81,994 | 9.36 | 605,940 | 1.27 |
| 100 | 130.0 | 9,069 | 371,291 | 2.44 | 1,261,027 | 0.72 |
| 90 | 117.0 | 20,606 | 6,279,485 | 0.33 | 3,320,332 | 0.62 |
| 80 | 104.0 | 92,189 | UNLIMITED | 0.00 | 15,721,676 | 0.59 |
| 70 | 91.0 | 1,018,852 | UNLIMITED | 0.00 | UNLIMITED | 0.00 |

2017 Calculation of Allowable Repetitions to Fatigue



- Simplifications
 - Assume axles act in isolation to each other
 - Assume strains linearly proportional to load
- Requires two response-to-load calculations



53 kN single axle/single tyres

2017 Calculation of Allowable Repetitions to Fatigue



For each axle group type and load level

- Predict strain under each isolated axle
- Use fatigue relationship to predict the allowable repetitions considering number of axles in the group

$$N_{ij} = \frac{1}{n} \times \frac{SF}{RF} \left[\frac{6918(0.856V_b + 1.08)}{E^{0.36} \mu \varepsilon_{ij}} \right]^5$$

| Axle group load (kN) | Expected group repetitions | Axles in group | Critical strain (microstrain) | Allowable group repetitions |
|-------------------------|-------------------------------|----------------|----------------------------------|--------------------------------|
| 10 | 3 740 | 2 | 10.9 | 3.29E+12 |
| 20 | 14 905 | 2 | 21.9 | 1.03E+11 |
| 30 | 16 167 | 2 | 32.8 | 1.35E+10 |
| 40 | 51 204 | 2 | 43.8 | 3.21E+09 |
| 50 | 168 246 | 2 | 54.7 | 1.05E+09 |
| 60 | 246 335 | 2 | 65.6 | 4.23E+08 |
| 70 | 283 346 | 2 | 76.6 | 1.96E+08 |
| 80 | 253 017 | 2 | 87.5 | 1.00E+08 |
| 90 | 197 125 | 2 | 98.4 | 5.57E+07 |
| 100 | 187 568 | 2 | 109.4 | 3.29E+07 |
| 110 | 162 315 | 2 | 120.3 | 2.04E+07 |
| 120 | 154 157 | 2 | 131.3 | 1.32E+07 |
| 130 | 152 240 | 2 | 142.2 | 8.86E+06 |



Concept of Standard Axle Repititions (SARs) Removed

Empirical design chart

- Permanent deformation

Mechanistic-empirical method

- Asphalt
- Cemented materials
- Lean-mix concrete
- Permanent deformation

ESA (as per 2012)

HVAGs & traffic load distribution HVAGs & traffic load distribution HVAGs & traffic load distribution ESA

$$N_{Standard Axle} = \left(\frac{9300}{\mu\varepsilon}\right)^7 \longrightarrow N_{ESA} = \left(\frac{9150}{\mu\varepsilon}\right)^7$$

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Example of Asphalt Thickness Changes



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Including lean-mix concrete

- Similar to asphalt, the use of the axle-strain method would have resulted in a general decrease in cemented materials thicknesses
- The thickness decrease varies with the traffic load distribution, being greater for distribution in which tandem axles and triaxles caused greater fatigue damage
- Experienced road agency practitioners advised:
 - they agreed the axle-strain method provided an improved method of assessing fatigue damage
 - but there was no evidence in support of a general reduction in cemented materials thickness

Overview of Part 2 changes

Flexible pavements

- Lime stabilised subgrades
- Cemented materials
- Lean-mix concrete
- Asphalt
- Design traffic
- Removal of Standard Axle Repetitions (SARs)
- Axle-strain method

Rigid pavements

• Joint detailing diagrams

Guide to Pavement Technology Part 4C Materials for Concrete Road Pavements

Introduction to team

Project Team

Austroads Project Manager Andrew Papacostas VicRoads

Project Leader Michael Moffatt ARRB

Team Member George Vorobieff Head to Head International

Review Team

Austroads Pavements Task Force

Stakeholders -Road & Traffic Authorities & Industry

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Key changes

- Diagrams updated and made consistent with Roads and Maritime Services (RMS) practice
- Reference made to geopolymer cements
- References updated
- Minor editorial changes

Questions?

Dr Michael Moffatt

National Technical Leader Pavements and Surfacings ARRB

P: +61 3 9881 1650

E: michael.moffatt@arrb.com.au

Upcoming Austroads webinar

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| Local Road Access for High Productivity Freight Vehicles | 27 March |
| Geopolymer Concrete and its Applications | 1 May |

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